SuDS Statement January 2020

EAS

Land at The Goat Public House 250 High Street Ponders End Enfield

Ponders End Properties Ltd

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1 Introduction

- 1.1 EAS has been commissioned to prepare a Sustainable Drainage Strategy to support a full planning application for the proposed extension and residential development at The Goat Public House, 250 High Street, Ponders End, Enfield, London EN3 4HB. A location plan is in **Appendix** A and the proposed development plans are in **Appendix B**.
- 1.2 The site comprises The Goat public house with the associated car park to the west of the building. The red line boundary covers 0.096 hectares (ha).
- 1.3 The contents of this SuDS statement are based on advice set out in The National Planning Policy Framework (NPPF), published February 2019; the Technical Guidance to the NPPF, published in July 2018; and the Planning Practice Guidance (PPG), published March 2014. Climate Change guidance published in February 2016 has also been considered.
- 1.4 This SuDS statement includes the following:
 - Assessment of existing surface water and groundwater flood risk within the site and discussion of any mitigation measures for the proposed development;
 - Consideration of the existing drainage arrangements and recommendations for the proposed surface water system to serve the site, including SuDS methods where possible;
 - Surface water drainage calculations for up to and including the 1 in 100 year event plus 40% as a proxy for future climate change impacts;
 - Existing and proposed discharge rates and volumes, the former comprising predevelopment greenfield runoff rates;
 - Drainage layout plan for the entire site, including the location of the point of discharge and any existing overland flow routes.
- 1.5 The information set out in this report demonstrates that the proposed development uses sustainable methods of drainage; will not increase the rate of surface water runoff; and will ensure that water leaving the site is not polluted with hydrocarbons or other potentially harmful chemicals.

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2 Policy Context

Introduction

2.1 This section sets out the policy context. The contents of this SuDS Statement are based on the advice set out in The National Planning Policy Framework (NPPF) published in July 2018 and the Planning Practice Guidance (PPG), published March 2014.

National Planning Policy Framework

2.2 Paragraph 164 footnote 50 of the NPPF states:

"A site-specific flood risk assessment should be provided for all developments in Flood Zones 2 and 3. In Flood Zone 1, an assessment should accompany all proposals involving: sites of 1 hectare or more; land which has been identified by the Environment Agency as having critical drainage problems; land identified in a strategic flood risk assessment as being at increased flood risk in future; or land that may be subject to other sources of flooding, where its development would introduce a more vulnerable use."

The flood zones are defined as:

- Flood Zone 1 Land assessed as having a less than 1 in 1,000 (<0.1%) annual probability of flooding from fluvial sources;
- Flood Zone 2 Land assessed as having between a 1 in a 100 and 1 in 1,000 (1% to 0.1%) annual probability of flooding from fluvial sources;
- Flood Zone 3a Land assessed as having a 1 in 100 or greater (>1%) annual probability of flooding from fluvial sources, or at least 0.5% annual probability of tidal flooding;
- Flood Zone 3b Land where water has to flow or be stored in times of flood.

2.3 Paragraph 155 discusses the suitability of development location, particularly with regards to future risks induced by climate change:

"Inappropriate development in areas at risk of flooding should be avoided by directing development away from areas at highest risk (whether existing or future). Where development is necessary in such areas, the development should be made safe for its lifetime without increasing flood risk elsewhere".

2.4 Paragraph 156 of the National Planning Policy Framework (NPPF) sets out how:

"Strategic policies should be informed by a strategic flood risk assessment, and should manage flood risk from all sources. They should consider cumulative impacts in, or affecting, local areas susceptible to flooding, and take account of advice from the Environment Agency and other relevant flood risk management authorities, such as lead local flood authorities and internal drainage boards".

2.5 Paragraphs 165 NPPF discusses the application of sustainable drainage systems:

"Major developments should incorporate sustainable drainage systems unless there is clear evidence that this would be inappropriate. The systems used should:

- Take account of advice from the lead local flood authority;
- Have appropriate proposed minimum operational standards;
- Have maintenance arrangements in place to ensure an acceptable standard of operation of the lifetime of the development; and
- Where possible, provide multifunctional benefits."
- 2.6 The EA Flood Map for Planning shows the site to be located entirely in Flood Zone 1, at 'Low' risk of flooding from fluvial sources. The EA Flood Map has been enclosed on **Appendix C**. This is considered to be an area with less than 1 in 1000 chance of flooding each year.

Non-Statutory Technical Standards for Sustainable Drainage Systems (2015)

2.7 This document published by Defra in March 2015 provides technical standards for SuDS systems, which should be used in conjunction with the NPPF and PPG. Standards include management of flood risk within and outside of the development; peak flow and volume control; construction and structural integrity; and designing for maintenance considerations. These have been considered in designing of the SuDS strategy for the site.

Local Policy

Enfield Council 2018-2036 New Local Plan

2.8 A new local plan is being produced and will address the main future challenges facing the borough including meeting housing needs, protecting the environment and renewing infrastructure.

London Borough of Enfield Local Flood Risk Management Strategy (March 2016)

- 2.9 Enfield Council is a Lead Local Flood Authority and has set out how they improve the management of local flood risk in their Local Flood Risk Management Strategy, published in March 2016. The site is approximately 650m north of the Boundary Ditch and not noted to be at significant risk of flooding from any source. It is noted that the number of properties at risk of flooding in Enfield is typically high compared to most other local authorities as most of the properties at risk are also located in the Lee Valley area, which was once a marshland. A wide range of flood defence measures are therefore necessary to manage the flood risk.
- 2.10 The largest recorded flood in Enfield was the 1947 River Lee event, which led to wide-spread flooding of the eastern half of the borough. The River Lee Flood Relief Channel was constructed in the 1970s to reduce the risk and flooding on this scale has not been experienced since.
- 2.11 Sustainable drainage measures (SuDS) are promoted in this document as an effective means of managing surface water runoff from new developments. Flood resilient construction methods are also highlighted as being suitable for new developments in flood risk areas.

London Plan

2.12 First published in 2004, the London Plan provides a strategic plan for London for the next 25 years. The London Plan provides a framework for economic, environmental, transport and social development. There have been numerous revisions to the original London Plan and a new London Plan is currently being drafted. The latest draft was published in July 2019.

2.13 Policy SI13 of the Draft New London Plan relates to Sustainable Drainage and states:

"A. Lead Local Flood Authorities should identify – through their Local Flood Risk Management Strategies and Surface Water Management Plans – areas where there are particular surface water management issues and aim to reduce these risks.

B. Development proposals should aim to achieve greenfield run-off rates and ensure that surface water run-off is managed as close to its source as possible in line with the following drainage hierarchy:

- rainwater harvesting (including a combination of green and blue roofs)
- infiltration techniques and green roofs
- rainwater attenuation in open water features for gradual release
- rainwater discharge direct to a watercourse (unless not appropriate)
- rainwater attenuation above ground (including blue roofs)
- rainwater attenuation below ground
- rainwater discharge to a surface water sewer or drain
- rainwater discharge to a combined sewer.

C. Development proposals for impermeable paving should be refused where appropriate, including on small surfaces such as front gardens and driveways.

D. Drainage should be designed and implemented in ways that address issues of water use efficiency, river water quality, biodiversity, amenity and recreation."

2.14 The proposed drainage strategy has considered the requirements of the London Plan and has been designed with this in mind.

3 Existing Site Assesment

Site Description

- 3.1 The development site is at The Goat Public House, 250 High Street, Ponders End, Enfield, London EN3 4HB. The site is located in the town centre, surrounded on the north, east and south by retail premises and other business uses. A large Tesco supermarket is around 120m to the north, and part of the Tesco's car park is located approximately 40m to the west of the site. Ponders End train station is located approximately 900m to the east. Residential dwellings are located away from the High Street, around 100m to the north east and south west of the site. A location plan is in **Appendix A**.
- 3.2 The existing site covers 0.096 hectares in area. The building is an existing public house with a courtyard, and will continue to function as a public house following the development. The car park is currently being used as a hand car wash and valeting centre.
- 3.3 The proposed scheme will include works to extend and refurbish the existing public house. The proposals also include an apartment block to provide 9 one- to three-bedroom flats along with associated car park and cycle parking area and front gardens.
- 3.4 Proposed development plans are included at Appendix B.

Local Watercourses

- 3.5 The closest watercourse is approximately 650m to the south of the site, and appears to be a culverted section of the Boundary Ditch.
- 3.6 The River Lee Navigation is around 1.15km to the east.

Site Levels

- 3.7 A topographical survey is enclosed in **Appendix D** but is to a local datum rather than Ordnance Datum. However, this can be used to determine the general falls across the site.
- 3.8 The highest part of the site is in the north west corner, where there are levels of around 10.15m. Ground levels drop to around 9.75m in the centre of the site before rising to around 9.85m along the southern boundary adjacent to Queensway.
- 3.9 It is noted from the Thames Water sewer records that the ground level along Queensway is approximately 17.30m AOD; however, this surface water drainage strategy has been based on the topographic survey levels.

Sewer Records

- 3.10 Thames Water sewer records are in **Appendix E**. These show a 225mm diameter Thames Water surface water sewer and foul sewer falling from west to east along Queensway. These sewers connect to surface water and foul sewers located in the High Street, which then fall to the south.
- 3.11 The sewer records indicate manhole 1901 and 1902 to the south west of the site. Surface water manhole 1902 does not have an associated invert level so it is not clear how deep this sewer

is. However, the foul manhole 1901 has both a cover level and invert level which suggests the invert is 1.97m below ground level.

Geology

- 3.12 With reference to the British Geological Survey online mapping, the site is located within an area with a bedrock of London Clay Formation Clay, Silt and Sand. Superficial deposits of Kempton Park Gravel Member Sand and Gravel are also recorded.
- 3.13 The presence of London Clay would not typically be favourable for formal infiltration drainage devices such as soakaways.
- 3.14 Historic borehole records taken around 200m south west of the site (labelled as TQ39NE480), taken in 1987, records groundwater at 4.70m below ground level. A historic borehole record taken 240m to the north in July 2006 records a groundwater level of 13.30m below datum. These records indicate the groundwater level is relatively deep in the local area so would be unlikely to pose a flood risk.

Existing Drainage

3.15 With reference to images on Google Streetview, the existing public house already has a surface water drainage system which directs roof runoff into gullies on the High Street. The topographic survey in **Appendix D** shows existing gullies in the car park to the west of the public house. As the existing car park is currently functioning as a hand car wash, it is assumed the gullies direct runoff to the public sewers nearby.

Surface Water Flood Risk

- 3.16 With reference to the surface water mapping on the GOV.UK website (<u>https://flood-warning-information.service.gov.uk/long-term-flood-risk/map</u>), the western side of the site which is currently the car park is in a 'Low' surface water flood risk area. 'Low' risk means the event does not occur often but the resulting flooding represents a 'worst case'. Depths of up to 300mm surface water are associated with this event. The vector mapping shows flowpaths to cross the car park and flow east along Queensway and then south down the High Street.
- 3.17 The surface water flood extent and flowpaths across the site disappear in the 'Medium' and 'High' risk events (i.e. the more frequent events which result in less flooding). The surface water maps have been included at **Appendix F**.
- 3.18 The surface water maps assume the sewer network is at capacity and water would be flowing across the site. The new SuDS system serving the proposed apartment block will provide attenuation volume for up to a 1 in 100 year (+40%CC) rainfall event, which would significantly reduce the surface water collecting in this area and flowing across the site.
- 3.19 The proposed finished floor levels on the ground floor of the new block should be raised 300mm above the external ground level. This will provide some protection against the overland flow route from offsite. If it is not possible to raise the ground floor levels, it is recommended that linear drains are located across the entrances to the ground floor apartments (particularly at the entrance to the garden area of Flat 1) to prevent overland flows from entering these dwellings.

4 Proposed Drainage Strategy

Pre-Development Runoff Rate

4.1 The site comprises the existing public house with a courtyard and car park to the west of the building which is currently being used as a hand car wash and valeting service.

Public House

4.2 The existing public house will be extended across the courtyard, which is already hardstanding and therefore drainage measures are already in place to serve this area. The existing building footprint/roof area is 289m², and with the extension this will increase to 296m². The increase is minimal and as the existing building already drains to the Thames Water public sewer in the High Street, this will; continue to be the case for the proposed public house. Therefore, the proposed extension has not been included in the new drainage strategy.

New Residential Block

- 4.3 The new apartment block is located on an area which is currently a car park and is laid to hardstanding. Gullies are already in place to manage runoff from this area. However, the new building will need a new drainage system to be included to serve the roof areas as well as the new hardstandings in a more sustainable way.
- Using the Modified Rational Method detailed in Butler, D and Davies, J. (2006), Urban Drainage,
 2nd ed., SPON, the surface water runoff for the existing impermeable areas of the car park,
 which totals 446m², has been calculated as follows:-

Q = CiA where Q = maximum flow rate (l/s) C= PIMP/PR i= rainfall intensity (mm/hr), A=area (ha)

- 4.5 It should be noted that a fixed rainfall intensity of 50mm/hr is used in this case, which has been recommended by Butler & Davies (2006) to avoid using inappropriately high intensities or very low concentration times, i.e. small sites.
- 4.6 Using the Modified Rationale Method (Butler and Davies, 2006), the total rate of runoff from the impermeable areas of the existing site is estimated to be **6.19 I/s**. The runoff calculations are enclosed in **Appendix G**.

Relevant SuDS Policy

- 4.7 SUDS mimic the natural drainage system and provide a method of surface water drainage which can decrease the quantity of water discharged, and hence reduce the risk of flooding. In addition to reducing flood risk, these features can improve water quality and provide biodiversity and amenity benefits.
- 4.8 The SUDS management train incorporates a hierarchy of techniques and considers all three SUDS criteria of flood reduction, pollution reduction, and landscape and wildlife benefit. In decreasing order of preference, the preferred means of disposal of surface water runoff is:

- Discharge to ground.
- Discharge to a surface water body.
- Discharge to a surface water sewer.
- Discharge to a combined sewer.
- 4.9 The philosophy of SUDS is to replicate as closely as possible the natural drainage from a site pre-development and to treat runoff to remove pollutants, resulting in a reduced impact on the receiving watercourses. The benefits of this approach are as follows:
 - Reducing runoff rates, thus reducing the flood risk downstream.
 - Reducing pollutant concentrations, thus protecting the quality of the receiving water body.
 - Groundwater recharge.
 - Contributing to the enhanced amenity an aesthetic value of development areas.
 - Providing habitats for wildlife in developed areas, and opportunity for biodiversity enhancement.

Site-Specific SuDS

4.10 The various SUDS methods need to be considered in relation to site-specific constraints. Several SUDS options are available to reduce or temporarily hold back the discharge of surface water runoff. Table 1 outlines the constraints and opportunities to each of the SUDS devices in accordance with the hierarchical approach outlined in The SUDS Manual CIRIA C753. It also indicates what could and could not be incorporated within the development, based upon site-specific criteria.

Device	Description	Constraints / Comments	Appropriate
Living roofs (source control)	Provide soft landscaping at roof level which reduces surface water runoff.	Not proposed due to pitch of roof.	No
Infiltration devices & Soakaways (source control)	Store runoff and allow water to percolate into the ground via natural infiltration.	The underlying geology is likely to have low permeability therefore formal infiltration devices would not be viable.	No
Pervious surfaces (source control)	Storm water is allowed to infiltrate through the surface into a storage layer, from which it can either infiltrate and/or slowly release to sewers.	The underlying geology is likely to have low permeability therefore formal infiltration devices are unlikely to be viable. However, permeable paving is proposed for the car park and access to provide some of the required attenuation volume, and will be unlined to allow for some infiltration to occur if possible.	Yes

Rainwater harvesting (source control)	Reduces the annual average rate of runoff from the Site by reusing water for non-potable uses e.g. toilet flushing, recycling processes.	Could potentially be used for each apartment although have assumed not for worst case scenario in terms of attenuation volume.	Possibly
Swales (permeable conveyance)	Broad shallow channels that convey / store runoff, and allow infiltration (ground conditions permitting).	Limited space within development boundary for swales.	No
Filter drains & perforated pipes (permeable conveyance)	Trenches filled with granular materials (to take flows from adjacent impermeable areas) that convey runoff while allowing infiltration.	Infiltration unlikely to be viable. A perforated pipe has been used to allow water to enter the permeable paving during extreme rainfall events.	Yes
Filter Strips (permeable conveyance)	Wide gently sloping areas of grass or dense vegetation that remove pollutants from run-off from adjacent areas.	Unlikely to be practical given the use of the development.	No
Infiltration basins (end of pipe treatment)	Depressions in the surface designed to store runoff and allow infiltration.	The underlying geology is unlikely to have the potential for infiltration due to low permeability.	No
Wet ponds & constructed wetlands (end of pipe treatment)	Provide water quality treatment & temporary storage above the permanent water level.	Limited space within development boundary for ponds and wetlands.	No
Attenuation Underground (end of pipe treatment)	Oversized pipes or geo-cellular tanks designed to store water below ground level.	Oversized pipes can be used to provide attenuation volume.	Yes

Table 1: Site Specific Sustainable Drainage

4.11 Given the local geology of London Clay, infiltration methods are not recommended. Instead, an attenuation and discharge system to a nearby sewer has been selected.

Proposed Discharge Rate

- 4.12 The existing public house and car park appears to discharge surface water runoff to the nearby Thames Water surface water sewer. As previously noted, the existing public house and courtyard already has a drainage system in place so the proposed extension to the public house has not been included in this drainage strategy as the impermeable area has not changed. The new extension will simply connect into the existing drainage system and no increase in discharge rate is anticipated as a result.
- 4.13 The proposed drainage system discussed here will serve the new apartment block and associated car park and access road. It is proposed that the new drainage system directs surface water runoff to the Thames Water surface water sewer in Queensway, but the discharge rate will be reduced to provide an improvement to the existing system.
- 4.14 WINDES MicroDrainage ICP SUDS method was used to determine the greenfield runoff rates for 1 hectare and scaled to the proposed impermeable area of 628m², which comprises the proposed roof area, car park and access road. The greenfield runoff rates are:
 - QBAR 3.9 l/s/ha (0.245 l/s)

- 1 in 1 year 3.3 l/s/ha (0.207 l/s)
- 1 in 30 year 8.9 l/s/ha (0.559 l/s)
- 1 in 100 year 12.5 l/s/ha (0.785 l/s)
- 4.15 The WINDES output it included in **Appendix H**.
- 4.16 The greenfield runoff rates for the proposed impermeable areas are very low and could result in blockages of the new drainage system. As the site is brownfield, it is instead proposed that a low runoff rate of **1.50 I/s** is used, which would provide an improvement on the existing discharge to the sewer, estimated to be around 6.19 I/s.
- 4.17 A pre-development enquiry was submitted to Thames Water to confirm they would accept the surface water discharge to their sewer at a discharge rate of 1.50 l/s and be able to accept the foul water flows from the 9 new apartments. Thames Water responded to confirm that there is sufficient capacity in their foul and surface water network to take flows from the proposed development. The Thames Water response is contained in **Appendix I**.

Proposed Drainage Strategy

- 4.18 Rainwater downpipes are not shown on the new building, therefore downpipe locations have been assumed based on the proposed roof plans in **Appendix B**.
- 4.19 It is proposed that rainwater downpipes will take roof runoff to a pipe network which will include a perforated pipe to let water back up into the permeable paving sub-base. This system will provide filtration and storage of the runoff.
- 4.20 It is anticipated that the permeable paving will be constructed using Grasscrete or similar, with attenuation volume provided in the sub-base.
- 4.21 The following typical construction would be expected for the permeable paving (based on guidance from Marshalls for the popular Priora Paving system):
 - 80mm paving course
 - 50mm laying course (generally a 6mm aggregate)
 - 80mm layer of perforated Asphalt Concrete (DBM)
 - A calculated depth of course grade aggregate (generally 250mm 350mm of a 30mm aggregate)
 - An additional sub-base / capping layer if required
- 4.22 Unlike other attenuation systems, the pollutants carried within the surface water run-off are filtered out as they pass through the course grade aggregate and sub-base. Once trapped they are then broken down over time; figures from the Construction Industry Research and Information Association have shown that 60-95% of suspended solids and 70-90% of hydrocarbons are removed by permeable pavements; as such no further filtration of pollutants will be required.
- 4.23 A perforated oversized pipe will be located within a trench below the sub-base of the permeable paving in the access road. This will enable runoff to back up within the perforated pipe and flow

into the permeable paving during extreme events, where it can be stored until it is discharged at a restricted rate to the surface water sewer in Queensway.

- 4.24 Oversized 300mm diameter pipes are used elsewhere in the proposed drainage network to provide the required attenuation volume to manage up to and including a 1 in 100 year (+40%CC) rainfall event.
- 4.25 The proposed pipe network was based on the topographic survey in **Appendix D** which is not to Ordnance Datum. The closest Thames Water surface water manhole in the Queensway does not have an associated invert level. Therefore, it was assumed that the surface water sewer invert level is 1.20m below the ground level of the road, based on the guidance in the publication 'Sewers for Adoption'. The ground level in the road was taken from the site-specific topographic survey.
- 4.26 The system was modelled in WINDES MicroDrainage and a minimum sub-base depth of 269mm would be required to provide the required attenuation volume for a 1 in 100 year (40%CC) rainfall event.
- 4.27 An orifice plate control would be at the downstream end of the perforated pipe, restricting the runoff to 1.50 l/s. A 27mm diameter orifice plate control with a suitable filter would be required to restrict the discharge rate.
- 4.28 The WINDES MicroDrainage results are included in **Appendix J** and the proposed SUDS strategy is in **Appendix K**.

Exceedance Flowpaths and Areas

4.29 In a storm event greater than that modelled, the capacity of the oversized pipes and permeable paving may become overwhelmed. In this instance, surface water runoff would pool in the shallower parts of the site, which would be along the proposed access road between manholes MH03 and MH04, and potentially also the proposed car park. As the site falls from north west to south east, the surface water would be directed towards the Queensway in this extreme event. It is also possible that overland flowpaths could develop along the western side of the site, as this is shown on the surface water mapping in **Appendix F**.

Maintenance of Development Drainage

4.30 All elements of the proposed drainage system will remain private and the responsibility for maintenance will be with the site owner or a maintenance company set up by the developer. Regular inspections of the permeable paving car park, outfall, catchpit and orifice plate control should be made, to ensure they are effective throughout the lifetime of the development and do not become blocked or damaged over time. Debris and silt should be removed from the catchpit and orifice plate regularly, especially following periods of heavy rainfall. It is likely that the Hydrobrake would come with a servicing package to ensure it would continue to work effectively. Some maintenance activities for the cellular storage crate detailed in CIRIA C753 'The SuDS Manual' are set out in Table 2.

Maintenance Schedule	Required Action	Frequency
Regular maintenance	Brushing and vacuuming.	Three times per year at end of winter, mid-summer, after autumn leaf fall, or as required based on site specific observations of clogging or manufacturer's recommendations.
Occasional maintenance	Stabilise and mow contributing and adjacent areas. Removal of weeds.	As required. As required.
Remedial actions	Remediate any landscaping which, through vegetation maintenance of soil slip, has been raised to within 50mm of the level of the paving. Remedial work to any depressions, rutting and cracked or broken blocks considered detrimental to the structural performance of a hazard to the user. Rehabilitation of surface and upper sub- surface.	As required As required As required (if infiltration performance is reduced as a result of significant clogging.)
Monitoring	Initial inspection Inspect for evidence of poor operation and/or weed growth. If required, take remedial action. Inspect silt accumulation rates and establish appropriate brushing frequencies. Monitor inspection chambers.	Monthly for 3 months after installation. 3 monthly, 48 hours after large storms. Annually.

Table 2: Maintenance tasks for permeable paving (Source: CIRIA C753, The SUDS Manual)

Manholes and Sewers/Oversized Pipe

- 4.31 Manhole covers should be lifted each year to remove visible debris and check for blockages it is suggested that this is undertaken every November after the heaviest leaf-fall has occurred.
- 4.32 Should a blockage occur at any time, it is advised to seek professional help to jet the drainage system to clean and clear the system.

Gutters and Downpipes

4.33 It is good practice to ensure that these are occasionally inspected to ensure they are in good order and free of leaves & debris. Once every 6 months should be sufficient.

5 Conclusions

- 5.1 The site is located entirely within Flood Zone 1 on the EA flood map, which indicates a 'low' risk of flooding from fluvial and tidal sources. 'Low' risk areas have an annual probability of flooding of less than 0.1% (or 1 in 1000 years).
- 5.2 The EA Flood Risk from Surface Water map is included shows that the western side of the site is at 'Low' risk of flooding, and up to 300mm surface water depth could occur. The overland flow routes appear to direct runoff into Queensway and towards the High Street. The 'Medium' and 'High' risk events do not show the site to flood.
- 5.3 There are Thames Water surface water and foul sewers in Queensway to the south of the site and in the High Street to the east. The existing public house and car park are likely to discharge unrestricted to these sewers.
- 5.4 The extension of the public house will be onto an area which is already impermeable, and the increase in roof area is minimal. Therefore, a new drainage strategy has not been designed to serve the new extension and the extended area will discharge to the existing surface water drainage system serving the public house.
- 5.5 The new apartment block and car park will have a new sustainable drainage system. The local geology suggests that infiltration methods would not be effective, so an attenuation method has been discussed with a restricted outfall to the Thames Water surface water sewer. The greenfield runoff rate from the site is very low, however as the site is brownfield an improvement can be made by restricting runoff to 1.50 l/s.
- 5.6 The proposed SuDS drainage strategy will direct roof runoff from all parts of the building into oversized pipes. The car park will be formed of permeable paving (Grasscrete or similar), and a perforated pipe will allow water to 'back up' into the permeable paving for additional storage. An orifice plate control will restrict the discharge rate to 1.50 l/s prior to discharge to the surface water sewer in Queensway.
- 5.7 This system was modelled in WINDES MicroDrainage for a 1 in 100 year (+40%CC) storm event and shown to work effectively. The reduction in runoff to the Thames Water surface water sewer will provide an improvement on the existing situation.
- 5.8 The proposed drainage system will remain private. Some management and maintenance tasks for permeable paving, oversized pipes and other elements of the drainage system have been described. It is recommended that regular inspections take place to ensure the drainage features remain effective.
- 5.9 To conclude, it is considered that development of the site with appropriate sustainable drainage features will provide the opportunity to reduce flood risk downstream in accordance with local plan policies.

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6 Appendices

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Appendix K - Proposed SUDS Strategy

Appendix: A – Location Plan



Appendix: B – Proposed Development Plans



01 Proposed - Basement Plan P/099 Scale 1:100@A1 1:200@A3





01 Proposed - Ground Floor Plan P/100 Scale 1:100@A1 1:200@A3

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Resi	idential Recycling a	nd Waste Stora	ge
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VINE92

Checked by

RPR

Revision

9

Drawn b

rawing No

P/100

1:100 @ A1 _{PJ}

1:200 @ A3

Ponders End Housing

GA Ground Floor Plan

23.10.2019

Drawing Name

Proposed









01 Proposed - Layout First Floor Plan P/101 Scale 1:100@A1 1:200@A3



Notes:

- This drawing is for planning purposes only





01 Proposed - GA Second Floor Plan P/102 Scale 1:100@A1 1:200@A3



Notes:

- This drawing is for planning purposes only









Notes:

- This drawing is for planning purposes only







01 Proposed - Residential Ground Floor Plan P/120 Scale 1:50@A1 1:100@A3



-(14)

15

-



01 Proposed - Residential First Floor Plan

P/121 / Scale 1:50@A1 1:100@A3





Notes:

- This drawing is for planning purposes only



(15)



01 Proposed - Residential Second Floor Plan

P/122 Scale 1:50@A1 1:100@A3





9

P/122

Second Floor Plan

-(14)



01 Proposed - Residential Roof Plan

P/123 Scale 1:50@A1 1:100@A3



-(14)

Tot Basement	70 sam
Existing basement (Retained)	70 sqm







03 Proposed - First Floor Plan

Scale 1:100@A1 1:200@A3

P/251







04 Proposed - Second Floor Plan Scale 1:100@A1 1:200@A3

Floor	253 sqm
in Store	10 sqm
ub Toilets	17 sqm
ub Kitchen	28 sqm
unction Room	n 68 sqm
Retained)	
Area	130 sqm

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Notes:

- This drawing is for planning purposes only

PROPOSED PUB AREA SCHEDULE GIA per Function (sqm)

Function

Existing Basement	70 sqm
Existing Pub Area and Toilets	130 sqm
Existing 1st Floor Pub Accommodation	94 sqm
Existing 2nd Floor Pub Accommodation	58 sqm
Proposed Function Room	68 sqm
Proposed Pub Kitchen	28 sqm
Proposed Toilets in Extension Area	17 sqm
Proposed Bar and Storage 1st Floor	30 sqm
Proposed Bin Store	10 sqm

TOTAL PROPOSED AREA

505 sqm



commodation	58 sqm
l Floor	58 sqm

















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Notes:

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PROPOSED RESIDENTIAL AREA SCHEDULE GIA Per Flat (sqm)

Flat	Туре	GF	1F	2F	Tot Area
FLAT 1	1b 2p	62	-	-	62 sqm
FLAT 2	1b 2p	-	32	27	59 sqm
FLAT 3	1b 2p	-	38	28	66 sqm
FLAT 4	3b 4p	73	26	-	99 sqm
FLAT 5	2b 4p	-	37	59	96 sqm
FLAT 6	1b 2p	46	19	-	65 sqm
FLAT 7	1b 2p	-	17	45	62 sqm
FLAT 8	3b 4p	69	23	-	92 sqm
FLAT 9	2b 4p	-	36	51	87 sqm

Total Flats Area

688 sqm

780 sqm

Total Circulation

52 sqm

Residential Cycle Parking Store	25 sqm
Residential Bin Store	15 sqm

TOTAL PROPOSED AREA



Revision	Description		Date	
7	Full Planning Application		23/10/2019	
6	Revised Planning Set		t	18/10/2019
5	Full Planning Applica		tion DRAFT	19/08/2019
4	Pre-P	anning Applica	tion	21/12/2018
3	Pre-A	oplication FINA	L DRAFT	18/12/2018
2	Pre-planning DRAFT			12/12/2018
1	Revised lift, bike store and		e and bin stores	28/11/2018
*	Proposed drawings DRAFT		RAFT	23/11/2018
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Date		Scale	Drawn by	Checked by
23.10.	2019	1:100 @ A1 1:200 @ A3	PJ	RPR
Drawing N	ame		Drawing No	Revision
Proposed Residential			_	

P/252

Accommodation schedule

7

ret Eloor	255 oam
on (1F)	27 sqm
2B/4p	36 sqm
3B/4p	23 sqm
1B/2p	17 sqm
1B/2p	19 sqm
2B/4p	37 sqm
3B/4p	26 sqm
1B/2p	38 sqm
1B/2p	32 sqm





01 Proposed - South Elevation P/301 / Scale 1:125@A1 1:250@A3





01 Proposed - Pub West Elevation P/310 / Scale 1:50@A1 1:100@A3





01 Proposed - Pub South Elevation P/311 Scale 1:50@A1 1:100@A3

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Client Name			
Ponders End Pr	operties LTD		
Project Name Ponders End Ho	ousing		Project Number
Date S	cale	Drawn by	Checked by
23.10.2019 1 Drawing Name	:50 @ A1 :100 @ A3	PJ Drawing No	RPR
Proposed Pub South Eleva	ation	P/311	6

Drawing Name
Proposed
Pub South Elevation







P/312

Pub East Elevation

6







Notes:

- This drawing is for planning purposes only

3 4 5m 0 2 Scalebar - 1:50 @ A1, 1:100 @ A3 Revision Description Date 7 Full Planning Application 23/10/2019 6 18/10/2019 Revised Planning Set 5 Full Planning Application DRAFT 19/08/2019 4 Planning Application FINAL DRAFT 19/06/2019 3 Pre-Planning Application 21/12/2018 2 Pre-Application FINAL DRAFT 18/12/2018 1 Pre-planning DRAFT 12/12/2018 Proposed drawings DRAFT 23/11/2018 Status O Vine/ Pre-Planning ٠ Planning Architecture Tender 0 Studio 0 Construction 0 As Built 132 Whitechapel Road, London E1 1JE www.vinearchitecture.com studio@vinearchitecture.com T 0207 377 5465 • Information 0 Discussion Client Name Ponders End Properties LTD Project Name Project Numbe Ponders End Housing VINE92 Checked by Drawn b 1:50 @ A1 PJ RPR 23.10.2019 1:100 @ A3

Revision

7

Drawing No

P/320

Drawing Name

Proposed

Residential West Elevation

+16.600












external cladding - natural tone

Double glazed doors (behind)

+15.650 SF Level 📿

Powder coated steel balustrade

+12.750

+9.850

external cladding - natural tone



















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Revision Description	on		Date	
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Ponders End	Properties LTD)		
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Ponders End	Housing		VINE92	
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23.10.2019	1:50 @ A1 1:100 @ A3	PJ	RPR	
Drawing Name		Drawing No	Revision	
Proposed Put Short Section	5 Extension	P/411	*	







Steel or Aluminium framed

Double glazed tophung window with timber or aluminium frames to match cladding or another neutral colour

Double glazed tophung window with timber or aluminium frames to match cladding or another neutral colour





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Appendix: C – EA Flood Map for Planning



Flood map for planning

Your reference **The Goat**

Location (easting/northing) 535187/196010

Created 7 Jan 2020 15:37

Your selected location is in flood zone 1, an area with a low probability of flooding.

This means:

- you don't need to do a flood risk assessment if your development is smaller than 1 hectare and not affected by other sources of flooding
- you may need to do a flood risk assessment if your development is larger than 1 hectare or affected by other sources of flooding or in an area with critical drainage problems

Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

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Appendix: D – Topographical Survey



PEL Eaves Level⁰17.882 PSV Stop Valve **9.938** PSV Stop Valve PBT 1pt BT Cover⁸9.865t BT Cover⁹9.916 PSP Sign Post°**9,773** 9.706 PBT 1pt BT Cover⁹9.864 9.387 PFH Fire Hydrant⁹9.830 9.404 PGU 1pt Gully⁹9.745 9.782 PMH 1pt Manhole PMH 1pt Manhole 9.726 9.695 9.747 9.747 **G**U 1pt Gully 9,723 9.794 PMH 1pt Manhole⁹.846 9.874 9.792 PLP Lamp Post⁹10,104 PTE Tree **12.256** Height (m): 12.000000 FE Fence 9.950 9.800 9.768 9.961 9.923 14.478 °9.706 13.572 9.782 17.224 18.432 °9.725 ◎ _◎ PB□ Bollard PB□ Bollard 18.37314 PCA Camera 15.709 PEL Eaves Level 20.394 9.777 ₀PGU 1pt Gully **9.736** 9.776 20.352 PGU 1pt Gully°**9.786** PEL Eaves Level 13.991 Eaves Level 13.994 °**9.77**2 913.561 PGU 1pt Gully**9.761** 10.003 PCA Camera °12.046 9.930 Bollard 18.193 19.415 PCA Camera °**9.78**3 °**9.948** 12.903 9.797 9.727 PBD Bollard 9.958 DO Door Opening ⁹.730 13.651 DD Door Opening **6780 Bollard 9.987** 9.797 PTE Tree **10.273** Helght (m): 13.500000 °**9.734 10.011** Bollard 12.554 9.7**2.7**61 9.953 PBD Bollard 9.891 13.492 PSP Sign Post[°]10.005 FE Fence String No. 5 9.912 String Hou 1 1151918 Eaves Level 16.227 PEL Eaves Level 16.248 PEL Eaves Level 17.393 10.140 PSP Sign Post 10.212 Height (m) 13.500000 12.185 10.128 °**9.6**67 °**9.815** 16.296 15.895 ¹2.000 9.682 9.750 9.724 PEL Eaves Level 16.190

PEL Eaves Level⁰16.917

PElpelovesdeved 105 BD Building 18.092 String No., 18



/ 9.435

PUC Undefined Cov^o9.817

Appendix: E – Thames Water Sewer Records



Based on the Ordnance Survey Map with the Sanction of the controller of H.M. Stationery Office, License no. 100019345 Crown Copyright Reserved

Thames Water Utilities Ltd, Property Searches, PO Box 3189, Slough SL1 4W, DX 151280 Slough 13 T 0845 070 9148 E searches@thameswater.co.uk I www.thameswater-propertysearches.co.uk

Manhole Reference	Manhole Cover Level	Manhole Invert Level
2011	n/a	n/a
201F	n/a	n/a
101B	n/a	n/a
101F	n/a	n/a
101A	n/a	n/a
101E	n/a	n/a
201B	n/a	n/a
291E	n/a	n/a
2907	17	15.68
2908	16.78	15.88
2909	16.74	14.71
2906	17.04	15.72
291A	n/a	n/a
2904	17.1	15.88
2905	17.38	16.09
2910	n/a	n/a
2001	17.24	16.09
2003	17 47	15.8
2005	17.46	15 99
201G	n/a	n/a
201H	n/a	n/a
2006	17 42	14 98
2002	17 47	16 55
201K	n/a	n/a
2008	17.48	15.82
2007	17.65	14 53
2010	n/a	n/a
2004	17.69	16.06
201D	n/a	n/a
29BD	n/a	n/a
291D	n/a	n/a
291D	n/a	n/a
29BC	n/a	n/a
291B	n/a	n/a
2902	17 24	15 64
2901	17.31	15.86
1902	17.31	n/a
2903	17.38	16.09
191B	n/a	n/a
1901	17.31	15.34
191A	n/a	n/a
001A	n/a	n/a
1001	n/a	n/a
0006	n/a	n/a
2022	n/a	n/a
1003	n/a	n/a
101D	n/a	n/a
1002	n/a	n/a
101C	n/a	n/a
201E	n/a	n/a
The position of the apparatus shown on this plan	is given without obligation and warranty, and the acc	curacy cannot be guaranteed. Service pipes are not

NB. Levels quoted in metres Ordnance Newlyn Datum. The value -9999.00 indicates that no survey information is available

The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

ALS Sewer Map Key



Sewer Fittings

A feature in a sewer that does not affect the flow in the pipe. Example: a vent is a fitting as the function of a vent is to release excess gas.

- Air Valve Dam Chase Fitting
- ≥ Meter

Π

0 Vent Column

Operational Controls

A feature in a sewer that changes or diverts the flow in the sewer. Example: A hydrobrake limits the flow passing downstream.

X Control Valve Ф Drop Pipe Ξ Ancillary Weir

Outfall

Inlet

Undefined End

End Items

いし

End symbols appear at the start or end of a sewer pipe. Examples: an Undefined End at the start of a sewer indicates that Thames Water has no knowledge of the position of the sewer upstream of that symbol, Outfall on a surface water sewer indicates that the pipe discharges into a stream or river.

Other Symbols

Symbols used on maps which do not fall under other general categories

- ****/ **** Public/Private Pumping Station
- * Change of characteristic indicator (C.O.C.I.)
- Ø Invert Level
- < Summit

Areas

Lines denoting areas of underground surveys, etc.

Agreement **Operational Site** :::::: Chamber Tunnel Conduit Bridge

Other Sewer Types (Not Operated or Maintained by Thames Water)



Notes:

hames

Water

- 1) All levels associated with the plans are to Ordnance Datum Newlyn.
- 2) All measurements on the plans are metric.
- 3) Arrows (on gravity fed sewers) or flecks (on rising mains) indicate direction of flow.
- 4) Most private pipes are not shown on our plans, as in the past, this information has not been recorded.
- 5) 'na' or '0' on a manhole level indicates that data is unavailable.
- 6) The text appearing alongside a sewer line indicates the internal diameter of the pipe in milimetres. Text next to a manhole indicates the manhole reference number and should not be taken as a measurement. If you are unsure about any text or symbology present on the plan, please contact a member of Property Insight on 0845 070 9148.

Thames Water Utilities Ltd, Property Searches, PO Box 3189, Slough SL1 4W, DX 151280 Slough 13 T 0845 070 9148 E searches@thameswater.co.uk I www.thameswater-propertysearches.co.uk



The position of the apparatus shown on this plan is given without obligation and warranty, and the accuracy cannot be guaranteed. Service pipes are not shown but their presence should be anticipated. No liability of any kind whatsoever is accepted by Thames Water for any error or omission. The actual position of mains and services must be verified and established on site before any works are undertaken.

Based on the Ordnance Survey Map with the Sanction of the controller of H.M. Stationery Office, License no. 100019345 Crown Copyright Reserved.

hames Water

ALS Water Map Key

Water Pipes (Operated & Maintained by Thames Water)

- 4" Distribution Main: The most common pipe shown on water maps. With few exceptions, domestic connections are only made to distribution mains.
- Trunk Main: A main carrying water from a source of supply to a 16" treatment plant or reservoir, or from one treatment plant or reservoir to another. Also a main transferring water in bulk to smaller water mains used for supplying individual customers.
- Supply Main: A supply main indicates that the water main is used 3" SUPPLY as a supply for a single property or group of properties.
- 3" FIRE Fire Main: Where a pipe is used as a fire supply, the word FIRE will be displayed along the pipe.
- Metered Pipe: A metered main indicates that the pipe in question 3" METERED supplies water for a single property or group of properties and that quantity of water passing through the pipe is metered even though there may be no meter symbol shown.
- Transmission Tunnel: A very large diameter water pipe. Most tunnels are buried very deep underground. These pipes are not expected to affect the structural integrity of buildings shown on the map provided.
- Proposed Main: A main that is still in the planning stages or in the process of being laid. More details of the proposed main and its reference number are generally included near the main.

PIPE DIAMETER	DEPTH BELOW GROUND
Up to 300mm (12")	900mm (3')
300mm - 600mm (12" - 24")	1100mm (3' 8")
600mm and bigger (24" plus)	1200mm (4')

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General PurposeValve Air Valve Pressure ControlValve Customer Valve **Hydrants** Single Hydrant Meters Meter End Items Symbol indicating what happens at the end of ^L Blank Flange Capped End Emptying Pit \cap

Valves



Operational Sites



Other Symbols

Data Logger

Other Water Pipes (Not Operated or Maintained by Thames Water)

Other Water Company Main: Occasionally other water company water pipes may overlap the border of our clean water coverage area. These mains are denoted in purple and in most cases have the owner of the pipe displayed along them.

Private Main: Indiates that the water main in guestion is not owned by Thames Water. These mains normally have text associated with them indicating the diameter and owner of the pipe.

Appendix: F – Surface Water Maps

EA Risk of Surface Water Flooding - Extent



Site Boundary

EA Risk of Surface Water Flooding – Low Risk Depth







EA Risk of Surface Water Flooding – Low Risk Velocity



Full ocreany Medium risk scenario Flood depth Aim (millimetres) NACE NEAD BLAC Mart Over 900mm Bis Depot. 300 to 900mm 20 (Below 300mm 0 PW Location you selected PW

EA Risk of Surface Water Flooding – Medium Risk Depth

Site Boundary



EA Risk of Surface Water Flooding – Medium Risk Velocity



Appendix: G – Existing Runoff Rates

Run-off from Existing Site

Methodology

Using the Modified Rational Method, the surface water run-off rate has been calculated for the existing impermeable areas of the car park.

Ref: Butler, D and Davies, J. (2006), Urban Drainage, 2nd ed, SPON.

Q = CiA

where

$$C = \frac{PIMP}{PR}$$

PIMP = Percentage of impervious area to total area PR = Percentage Runoff

	Surface Area (m ²)
Existing Impervious Areas	446
Total Area	446

i (Rainfall intensity, mm/hr) =	50.00
i (Rainfall intensity, m/hr) =	0.050
i (Rainfall intensity, m/s) =	1.38 x 10⁻⁵

Percentage run-off (PR)

Existing Impervious Area = 100%

Percentage of impervious area to total area (PIMP) PIMP = 446/446 = 100%

Therefore C = $\frac{PIMP}{PR}$ = 1

Runoff from existing site: Q = CiA $Q = 1 \times 1.38 \times 10^{-5} \times 446m^2$ $Q = 0.006194m^3s^{-1}$ $Q = 6.19 ls^{-1}$

Total Q for the existing site = 6.19 ls⁻¹

Appendix: H – Greenfield Runoff Rates

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ICP SUDS Mean Annual Flood

Input

Return Period (years) 100 Soil 0.450 Area (ha) 1.000 Urban 0.000 SAAR (mm) 633 Region Number Region 6

Results 1/s

QBAR Rural 3.9 QBAR Urban 3.9 Q100 years 12.5 Q1 year 3.3 Q30 years 8.9 Q100 years 12.5

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Appendix: I – Thames Water Pre-Development Enquiry



Louisa Wade

EAS Unit 23 The Maltings Stanstead Abbotts Hertfordshire SG12 8HG Wastewater pre-planning Our ref DS6069325

20 January 2020

Pre-planning enquiry: Capacity Confirmation

Site: The Goat, 250 High Street, Enfield EN3 4HB

Dear Louisa,

Thank you for providing information on your development.

Proposed site: Flats (9 units) Proposed foul water to discharge by gravity via manhole TQ35951901 Proposed surface water to discharge at 1.50 l/s for all storm events up to and including 1:100yr+40%CC into 225mm surface water sewer on Queensway.

We have completed the assessment of the foul water flows and surface water run-off based on the information submitted in your application with the purpose of assessing sewer capacity within the existing Thames Water sewer network.

We're pleased to confirm that there will be sufficient foul and surface water capacity in our sewerage network to serve your development.

This confirmation is valid for 12 months or for the life of any planning approval that this information is used to support, to a maximum of three years.

Please note that you must keep us informed of any changes to your design – for example, an increase in the number or density of homes. Such changes could mean there is no longer sufficient sewerage capacity.

What happens next?

Please make sure you submit your connection application, giving us at least 21 days' notice of the date you wish to make your new connection/s.



If you have any further questions, please contact me on 020 3577 9224.

Yours sincerely

meli

Hemlata Gurung Technical Coordinator Developer Services – Sewer Adoptions Team Appendix: J - WINDES MicroDrainage Results

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	Exist	ing Net	work I	Details	s for	r Exis	sting			
PN	Length Fal	l Slope	I.Area	T.E.	в	ase	k	HYD	DIA	
	(m) (m)	(1:X)	(ha)	(mins)	Flow	(1/s)	(mm)	SECT	(mm)	
1 000		1 1 7 0 5	0 005	5 00		0 0	0 6 0 0		200	
1.000	6.900 0.04	10 1/2.5	0.005	5.00		0.0	0.600	0	300	
1.001	14.200 0.06	50 236.7	0.012	0.00		0.0	0.600	0	300	
2.000	11.700 0.05	50 234.0	0.007	5.00		0.0	0.600	0	300	
2.001	19.900 0.08	30 248.8	0.000	0.00		0.0	0.600	0	300	
2.002	5.200 0.05	50 104.0	0.005	0.00		0.0	0.600	0	300	
1.003	5.000 0.05	50 100.0	0.022	0.00		0.0	0.600	0	150	
		Net	work Re	esults	Tab	le				
	PN	US/IL Σ	I.Area	Σ Bas	se	Vel	Cap			
		(m)	(ha)	Flow (1/s)	(m/s)	(1/s)			
	1 000	8 800	0 005		0 0	1 19	84 4			
	1.000	8.760	0.003		0.0	1.09	77.2			
	1.002	8.710	0.029		0.0	1.02	71.9			
	2.000	8.830	0.007		0.0	1.02	72.3			
	2.001	8 700	0.007		0.0	1 54	109 0			
	2.002	0.700	0.012		0.0	1.01	103.0			
	1.003	8.650	0.063		0.0	1.00	17.8			

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Micro Drainage	Network 2013.1.1	

Manhole Schedules for Existing

MH Name	MH CL (m)	MH Depth (m)	MH Connection	MH Diam.,L*W (mm)	PN	Pipe Out Invert Level (m)	Diameter (mm)	PN	Pipes In Invert Level (m)	Diameter (mm)	Backdrop (mm)
MUO1	9 900	1 100	Open Manhele	1200	1 000	<u> </u>	300				
MHUI	9.900	1.100	open Mannore	1200	1.000	0.000	500				
MH02	9.900	1.140	Open Manhole	1200	1.001	8.760	300	1.000	8.760	300	
MH03	9.900	1.190	Open Manhole	1200	1.002	8.710	300	1.001	8.710	300	
MH05	10.010	1.180	Open Manhole	1200	2.000	8.830	300				
MH06	9.970	1.190	Open Manhole	1200	2.001	8.780	300	2.000	8.780	300	
MH07	9.800	1.100	Open Manhole	1200	2.002	8.700	300	2.001	8.700	300	
MH04	9.900	1.250	Open Manhole	1200	1.003	8.650	150	1.002	8.650	300	
								2.002	8.650	300	
	9.900	1.300	Open Manhole	0		OUTFALL		1.003	8.600	150	

EAS									Page 3		
Unit 1	08 T1	he Mal	ting	s					10		
Stanst	ead Al	bbotts							TY7	Para	and a
Hertfo	rdshi	re SG	12 81	HG					Ly .	Tand	
Date 1	Date 16/01/2020 15:10					Designed by Maz				ETT.	ROP
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Micro	Draina	age		1	Network 2013.1.1						
				PIPE	ELINE SC	HEDULES	5 for H	Exist	ing		
					Upst	tream M	anhole				
	PN	Hyd	Diam	МН (C.Level I	.Level D	.Depth	1	MH	MH DIAM.,	L*W
		Sect	(mm)	Name	(m)	(m)	(m)	Conn	ection	(mm)	
	1.000	0 0	300	MH01	9.900	8.800	0.800	Open 1	Manhole		1200
	1.001	1 o	300	MH02	9.900	8.760	0.840	Open 1	Manhole		1200
	1.002	2 0	300	MH03	9.900	8.710	0.890	Open 1	Manhole		1200
	2 000		300	МНОБ	10.010	8,830	0 880	Open 1	Manhole		1200
	2.001	1 0	300	MH06	9.970	8.780	0.890	Open 1	Manhole		1200
	2.002	2 0	300	MH07	9.800	8.700	0.800	Open 1	Manhole		1200
		2	150		0.000	0.055		<u>_</u>			1000
	1.003	3 0	150	MH04	9.900	8.650	1.100	Open 1	Manhole		1200
					Downs	stream 1	Manhol	e			
	PN	Length (m)	Slope (1:X)	e MH Name	C.Level (m)	I.Level (m)	D.Depti (m)	h Con	MH	MH DIAM (mm	., L*W)
	1 000	<	170 1		0 000	0 760	0.04	0.0	Marchalla		1000
	1 001	6.900	206 () MH02	9.900	8.760	0.84	0 Oper 0 Oper	Mannole Manhole		1200
	1.002	14.200	236.	7 MH04	9.900	8.650	0.95	0 Open	Manhole		1200
	2.000	11.700	234.0) MH06	9.970	8.780	0.89	0 Oper	Manhole		1200
	2.001	19.900	248.8	3 MH0/) MH0/	9.800	8.700	0.80	0 Oper	Manhole Manhole		1200
	2.002	J.200	104.0	J 141104	9.900	0.000	0.95	o oper	i Mannoite		1200
	1.003	5.000	100.0)	9.900	8.600	1.15	0 Oper	Manhole		0
			Free	Flow	ving Out	fall De	etails	for i	Existin	đ	
		O	utfall	. Ou	tfall C.	Level I.	Level	Mir	n D,L	W	
		Pip	e Numb	er N	Name	(m)	(m)	I. Le	vel (mm)	(mm)	
								(m)			
			1.0	03		9.900	8.600	0.	000 0	0	
				~ ·		~ • • •	-	_ ·			
				Simu	⊥ation (Criteri	a for	Exist	ing		
		Volumet	ric P	unoff	Coeff 0	750 자식	ditiona	1 5100	7 _ ♀ ^f	Total El	
		Areal	Reduc	tion F	Factor 1.	, JU Ad 000	MADD	Factor	, – 5 Oľ : * 10m³/	'ha Storad	ge 2.000
		041	Hot S	tart	(mins)	0			Inlet Co	effiecier	nt 0.800
		Hot	Start	Level	l (mm)	0 Flow	per Pe	rson p	per Day	l/per/day	y) 0.000
Ma	anhole	Headlos	ss Coe	ff (Gl	lobal) 0.	500			Run 1	lime (mins	s) 60
	Foul S	ewage p	per he	ctare	(l/s) 0.	000		Outp	out Inter	rval (mins	s) 1
		Numbe	r of '	Inpu+	Hvdrogram	hs () Num	nber of	Stora	ge Struc	tures 1	
		Num	ber of	E Onli	ne Contro	ols 1 Num	nber of	Time/	Area Dia	grams 0	
		Numb	er of	Offli	ne Contro	ols O Num	nber of	Real	Time Con	trols O	

Synthetic Rainfall Details

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Micro Drainage	Network 2013.1.1	
Sim	ulation Criteria for E	xisting
Rainfall Mod	lel FSR	Profile Type Summer
Recuiii Feriou (year Regi	on England and Wales	Cv (Winter) 0.840
M5-60 (m	um) 20.000 Storn	n Duration (mins) 30
Ratic	R 0.450	
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Online Controls for Existing

Orifice Manhole: MH04, DS/PN: 1.003, Volume (m³): 2.6

Diameter (m) 0.027 Discharge Coefficient 0.600 Invert Level (m) 8.650

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Storage Structures for Existing

Porous Car Park Manhole: MH04, DS/PN: 1.003

Infiltration Coefficient Base (m/hr)	0.00000	Width (m)	14.7
Membrane Percolation (mm/hr)	1000	Length (m)	14.7
Max Percolation (1/s)	60.0	Slope (1:X)	100.0
Safety Factor	2.0	Depression Storage (mm)	5
Porosity	0.30	Evaporation (mm/day)	3
Invert Level (m)	9.300	Cap Volume Depth (m)	0.000

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Summary of Critical F	Results by Maximum Outflo	w (Rank 1) for Existing		
Areal Reduction Hot Start Hot Start Lev Manhole Headloss Coeff Foul Sewage per hectar	Simulation Criteria n Factor 1.000 Additional Fl c (mins) 0 MADD Fact rel (mm) 0 (Global) 0.500 Flow per Person re (1/s) 0.000	ow - % of Total Flow 0.000 or * 10m³/ha Storage 2.000 Inlet Coeffiecient 0.800 per Day (l/per/day) 0.000		
Number of Inpu	t Hydrographs () Number of Sto	rage Structures 1		
Number of On	line Controls 1 Number of Tim	e/Area Diagrams 0		
Number of Off	line Controls 0 Number of Rea	l Time Controls O		
Rainfall	<u>Synthetic Rainfall Details</u> Model FSR R	atio R 0.450		
R	egion England and Wales Cv (S	ummer) 0.750		
M5-60	(mm) 20.000 CV (W	inter) 0.840		
Margin for Flo	bod Risk Warning (mm) 300.0	DVD Status OFF		
	Analysis Timestep Fine Ir	ertia Status OFF		
	bib beacas on			
Profile(s) Summer and Winter Duration(s) (mins) 15, 30, 60, 120, 240, 360, 480, 960, 1440 Return Period(s) (years) 1, 30, 100 Climate Change (%) 0, 0, 40				
Ret	curn Climate First X Firs	t Y First Z O/F Lvl		
PN Storm Per	riod Change Surcharge Flo	od Overflow Act. Exc.		
1.000 15 Winter	100 +40% 30/15 Summer			
1.001 15 Winter	100 +40% 30/15 Summer			
1.002 15 Winter 2.000 15 Winter	100 +40% 30/15 Summer 100 +40% 30/15 Winter			
2.000 15 Winter	100 +40% 30/15 Summer			
2.002 15 Winter	100 +40% 30/15 Summer			
1.003 120 Winter	100 +40% 1/15 Summer			
Water	Flooded	Pipe		
US/MH Level	Surch'ed Volume Flow / O'f	low Flow		
PN Name (m)	Depth (m) (m^3) Cap. (1)	's) (1/s) Status		
1.000 MH01 9.468	0.368 0.000 0.03	0.0 2.1 SURCHARGED		
1.001 MH02 9.468	0.408 0.000 0.13	0.0 7.8 SURCHARGED		
1.002 MH03 9.467 2.000 MH05 9.467	0.457 0.000 $0.230.337$ 0.000 0.05	U.U I3.6 SURCHARGED 0.0 3.1 SURCHARGED		
2.000 MH06 9.467	0.387 0.000 0.04	0.0 2.4 SURCHARGED		
2.002 MH07 9.466	0.466 0.000 0.06	0.0 3.9 SURCHARGED		
1.003 MH04 9.601	0.801 0.000 0.11	0.0 1.5 FLOOD RISK		
	1000 0010 Mi D	T+d		
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Appendix K - Proposed SUDS Strategy

SuDS Statement and Drainage Strategy |The Goat, Ponders End, Enfield



	KEY:					
	217sqm PERMEABLE PAVING (GRASSCRETE OR SIMILAR)					
	300mm ø PERFORATED PIPE					
	300mm ø OVERSIZED PIPE					
	\bigcirc	МА	NHOLE CHAMBER			
	EXISTING THAMES WATER SURFACE WATER SEWER					
•						
\setminus	REV DATE	BY	DESCRIPTION		СНК	APD
	DRAWING STATUS:				L	
	Ordnance Survey (c) Crown Copyright 2018. All rights reserved. Licence number 100022432					
	EAS					
	Unit 23, ⁻	The Malti	ngs, Stanstead Abbotts, He Tel: 01920 871777	rtfordshire, SG	12 8HG	;
			www.eastp.co.uk			
	CLIENT:		s end properti	ES LTD		
	VINE ARCHITECTURE STUDIO					
	THE GOAT PUBLIC HOUSE 250 HIGH STREET ENFIELD					
_	TITLE:					
		PROPO	DSED SUDS STRA	TEGY		
	SCALE @ A3:		DESIGN-DRAWN:	DATE:		
	1:200		LW	16.01	1.20	
	PRUJECT No:		URAWING No:	11		
	2564 SK01					